

# *Lecture 10*

## *AO Control Theory*



Claire Max  
with thanks to Don Gavel and Don Wiberg  
UC Santa Cruz  
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# *What are control systems?*

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- Control is the process of making a system variable adhere to a particular value, called the reference value.
- A system designed to follow a changing reference is called tracking control or servo.

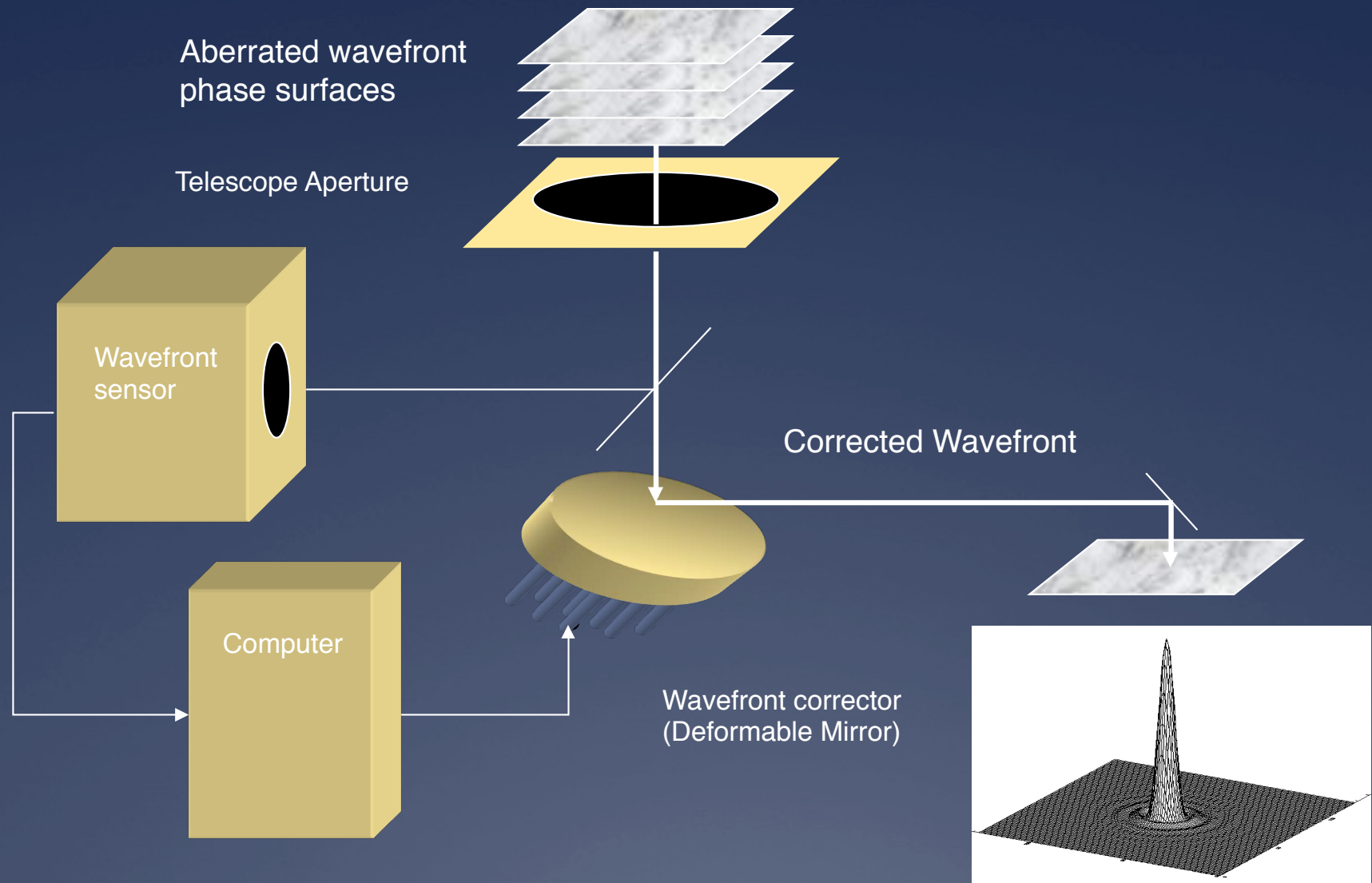
# Outline of topics

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- What is control?
  - The concept of closed loop feedback control
- A basic tool: the Laplace transform
  - Using the Laplace transform to characterize the time and frequency domain behavior of a system
  - Manipulating *Transfer functions* to analyze systems
- How to predict performance of the controller

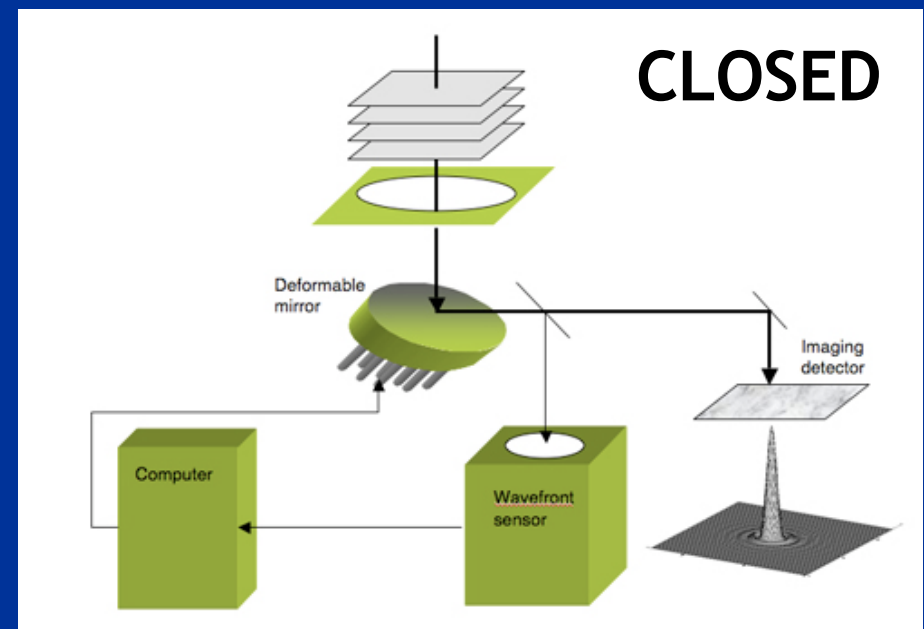
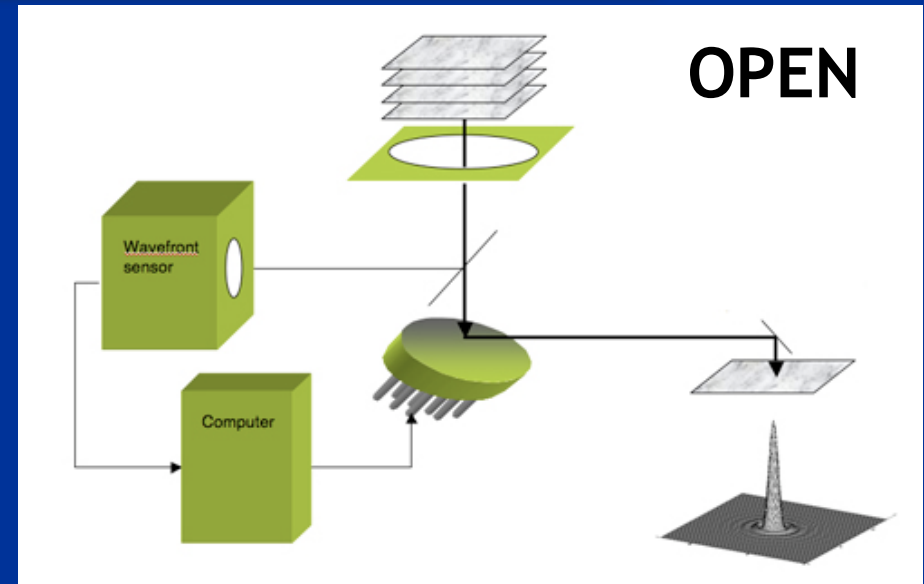
# Adaptive Optics Control



# Differences between open-loop and closed-loop control systems



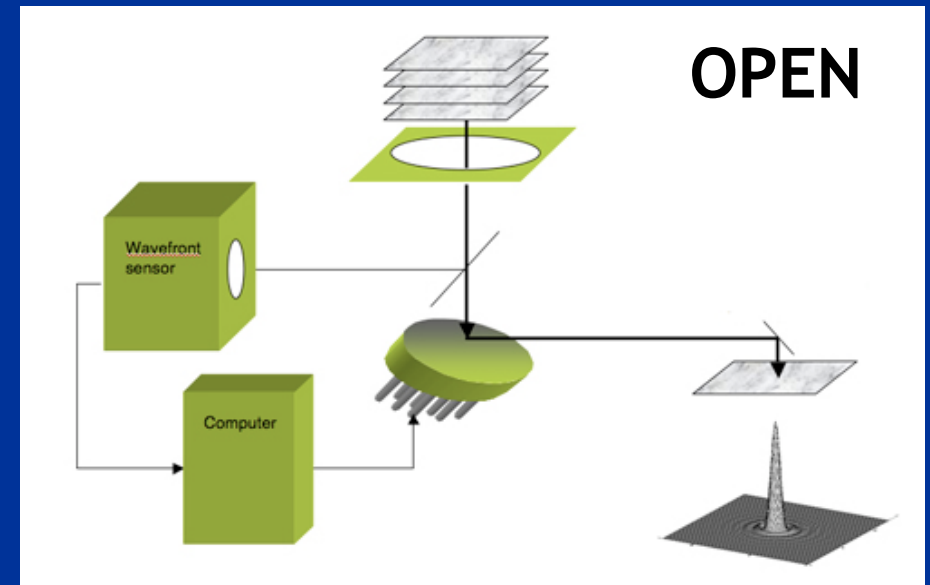
- Open-loop: control system uses no knowledge of the output
- Closed-loop: the control action is dependent on the output in some way
- “Feedback” is what distinguishes open from closed loop
- What other examples can you think of?



# More about open-loop systems



- Need to be carefully calibrated ahead of time:
- Example: for a deformable mirror, need to know exactly what shape the mirror will have if the  $n$  actuators are each driven with a voltage  $V_n$
- Question: how might you go about this calibration?



# *Some Characteristics of Closed- Loop Feedback Control*

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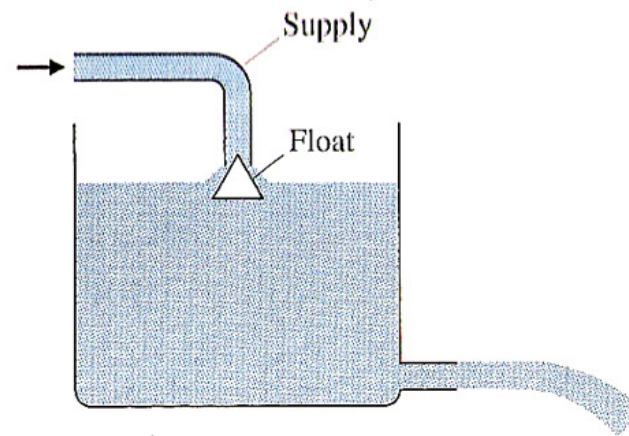
- Increased accuracy (gets to the desired final position more accurately because small residual errors will get corrected on subsequent measurement cycles)
- Less sensitivity to nonlinearities (e.g. hysteresis in the deformable mirror) because the system is always making small corrections to get to the right place
- Reduced sensitivity to noise in the input signal
- BUT: can be unstable under some circumstances (e.g. if gain is too high)

# Historical control systems: float valve



**Figure 1.7**

Early historical control of liquid level and flow

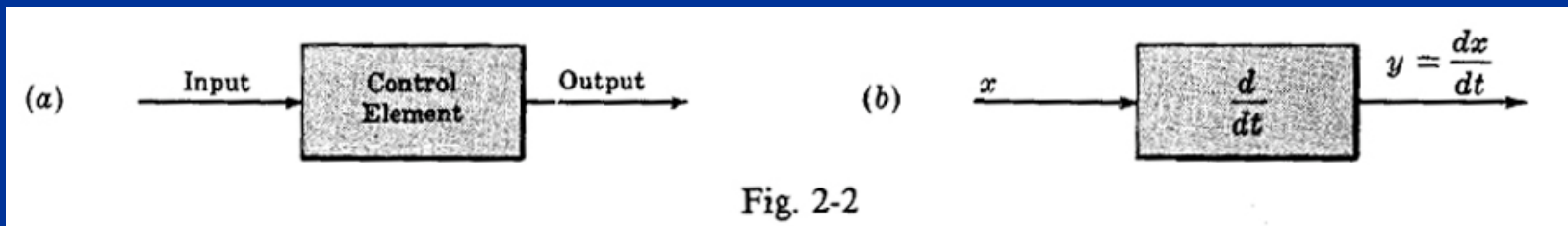


Credit: Franklin, Powell, Emami-Naeini

- As liquid level falls, so does float, allowing more liquid to flow into tank
- As liquid level rises, flow is reduced and, if needed, cut off entirely
- Sensor and actuator are both “contained” in the combination of the float and supply tube



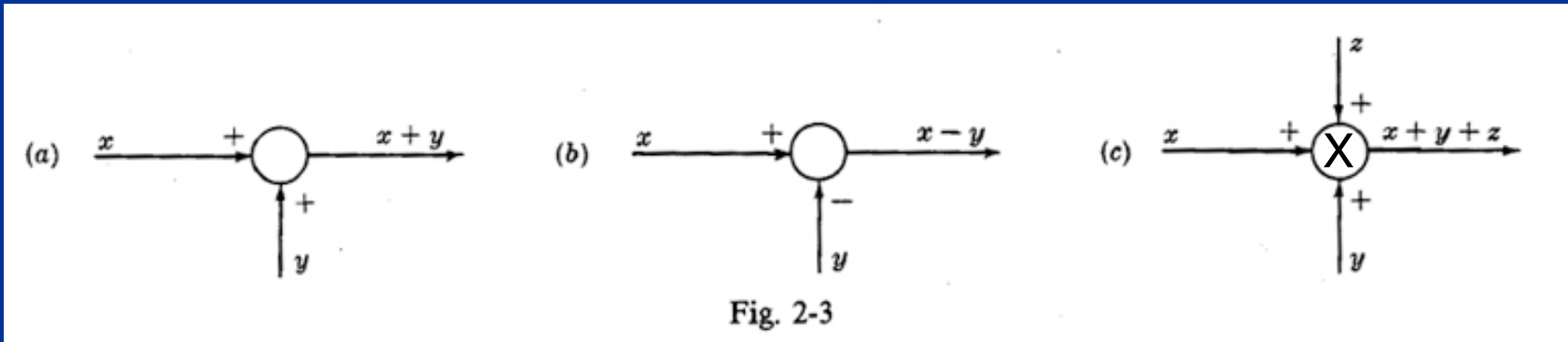
# Block Diagrams: Show Cause and Effect



Credit: DiStefano et al. 1990

- Pictorial representation of cause and effect
- Interior of block shows how the input and output are related.
- Example (b) output is the time derivative of the input

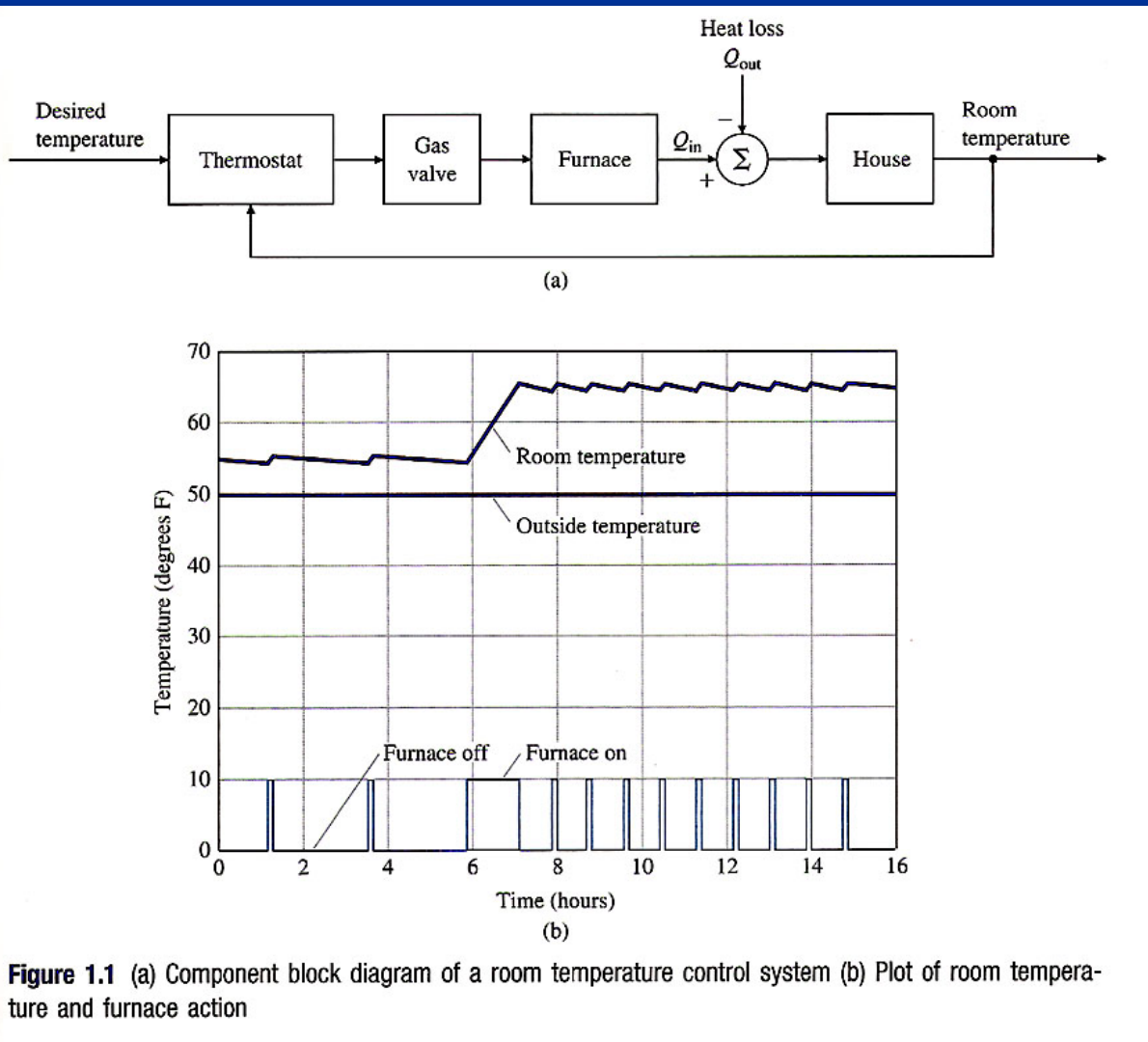
# “Summing” Block Diagrams are circles



Credit: DiStefano et al. 1990

- Block becomes a circle or “summing point”
- Plus and minus signs indicate addition or subtraction (note that “sum” can include subtraction)
- Arrows show inputs and outputs as before
- Sometimes there is a cross in the circle

# A home thermostat from a control theory point of view

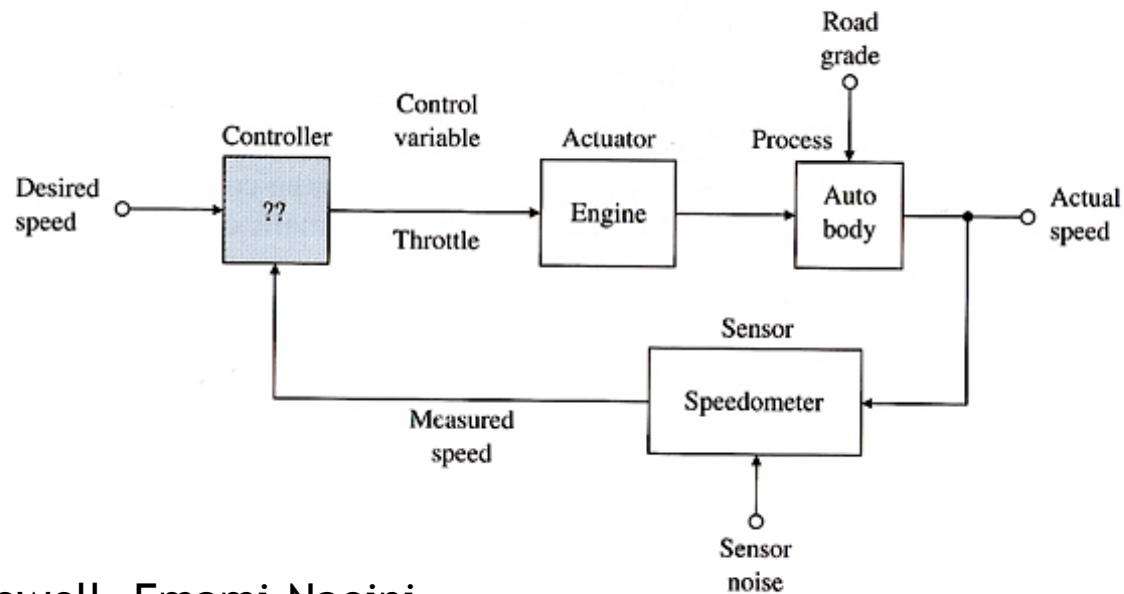


**Figure 1.1** (a) Component block diagram of a room temperature control system (b) Plot of room temperature and furnace action

# Block diagram for an automobile cruise control



**Figure 1.3**  
Component block diagram  
of automobile cruise control



Credit: Franklin, Powell, Emami-Naeini

## Example 1

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- Draw a block diagram for the equation

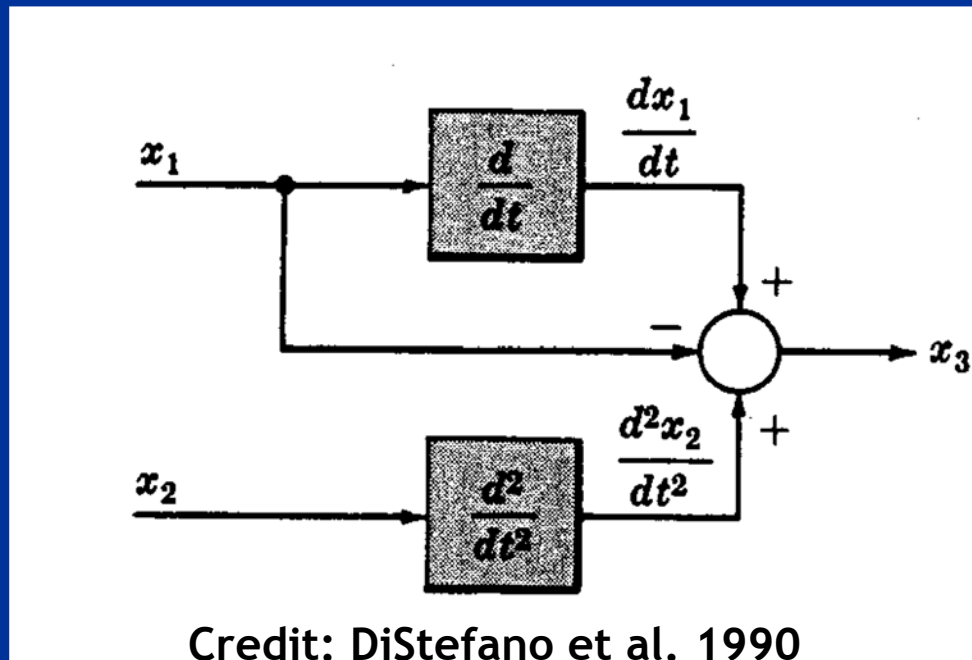
$$x_3 = \frac{d^2x_2}{dt^2} + \frac{dx_1}{dt} - x_1$$

# Example 1



- Draw a block diagram for the equation

$$x_3 = \frac{d^2x_2}{dt^2} + \frac{dx_1}{dt} - x_1$$



## Example 2

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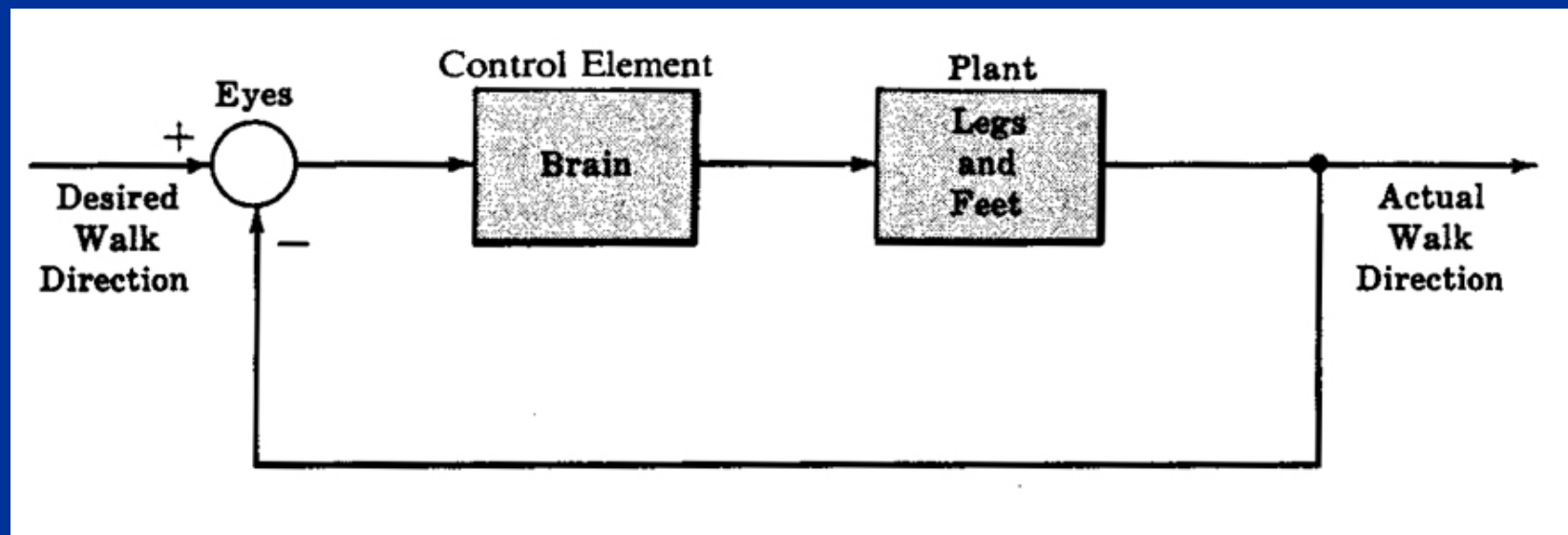


- Draw a block diagram for how your eyes and brain help regulate the direction in which you are walking

## Example 2



- Draw a block diagram for how your eyes and brain help regulate the direction in which you are walking



Credit: DiStefano et al. 1990



## *Summary so far*

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- Distinction between open loop and closed loop
  - Advantages and disadvantages of each
- Block diagrams for control systems
  - Inputs, outputs, operations
  - Closed loop vs. open loop block diagrams

## The Laplace Transform Pair

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$$H(s) = \int_0^{\infty} h(t) e^{-st} dt$$

$$h(t) = \frac{1}{2\pi i} \int_{-i\infty}^{i\infty} H(s) e^{st} ds$$

- Similar in some ways to Fourier Transform, but for initial value problems where you want to see the time evolution
- By contrast, Fourier Transform deal with periodic systems

# Laplace Transform Pairs



	$h(t)$	$H(s)$
unit step		$\frac{1}{s}$
	$e^{-\sigma t}$	$\frac{1}{s + \sigma}$
	$e^{-\sigma t} \cos(\omega t)$	$\frac{1}{2} \left( \frac{1}{s + \sigma - i\omega} + \frac{1}{s + \sigma + i\omega} \right)$
	$e^{-\sigma t} \sin(\omega t)$	$\frac{1}{2i} \left( \frac{1}{s + \sigma - i\omega} - \frac{1}{s + \sigma + i\omega} \right)$
delayed step		$\frac{e^{-sT}}{s}$
unit pulse		$\frac{1 - e^{-sT}}{s}$

## Laplace Transform Properties

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$$L\{ \alpha h(t) + \beta g(t) \} = \alpha H(s) + \beta G(s)$$

Linearity

$$L\{ h(t + T) \} = e^{sT} H(s)$$

Time-shift ( $T \leq 0$ )

$$L\{ \delta(t) \} = 1$$

Dirac delta function transform  
("sifting" property)

$$L\left\{ \int_0^t h(t') g(t - t') dt' \right\} = H(s) G(s)$$

Convolution

$$L\left\{ \int_0^t h(t') \delta(t - t') dt' \right\} = H(s)$$

Impulse response

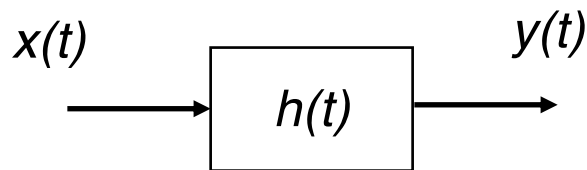
$$\int_0^t h(t - t') e^{i\omega t'} dt' = H(i\omega) e^{i\omega t}$$

Frequency response

# System Block Diagrams

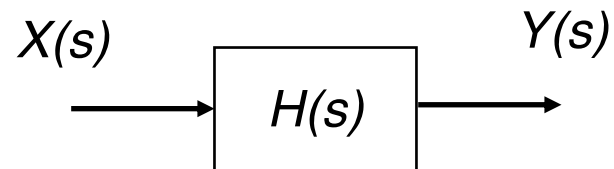


Time domain



**Convolution** of input  $x(t)$   
with impulse response  $h(t)$

Frequency domain

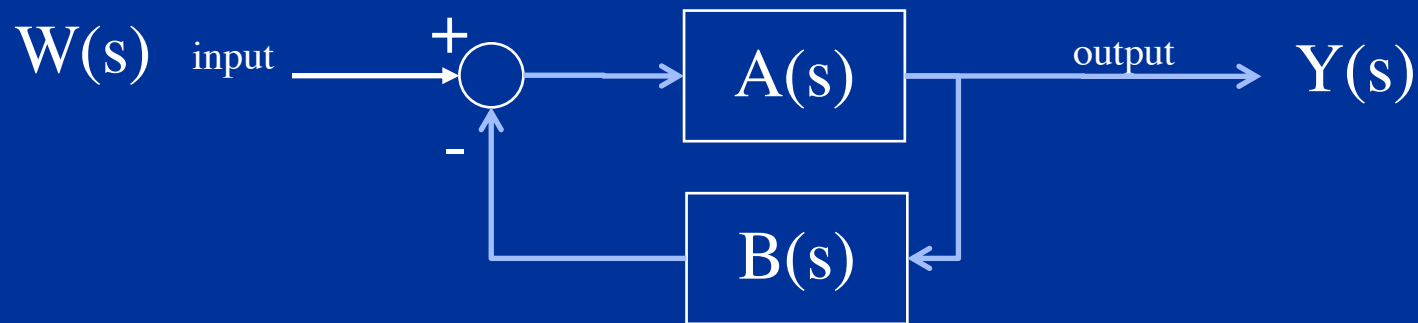


- **Product** of input spectrum  $X(s)$  with frequency response  $H(s)$
- $H(s)$  in this role is called the *transfer function*

$$L \left\{ \int_0^t h(t') x(t-t') dt' \right\} = H(s) X(s) = Y(s)$$



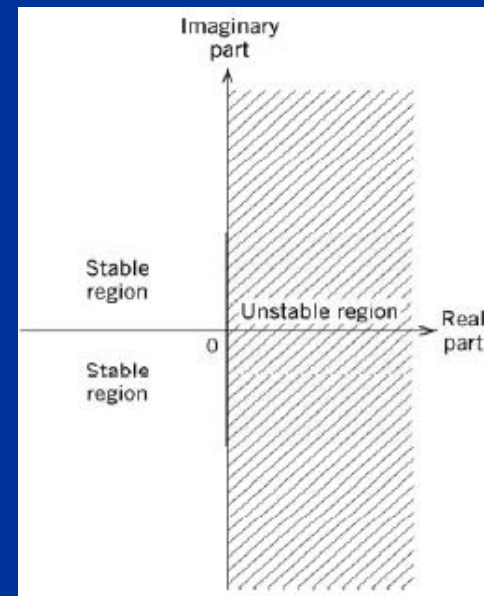
# Control Loop Arithmetic



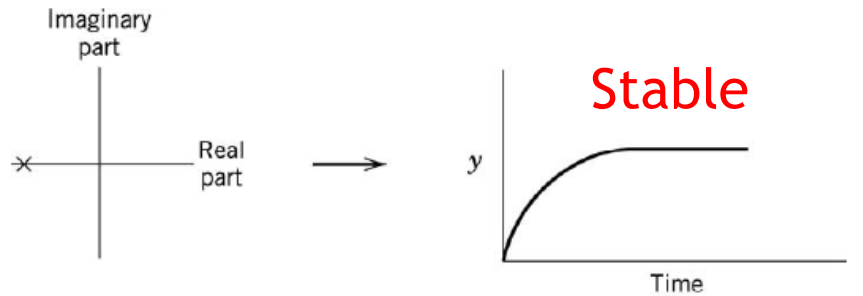
$$Y(s) = A(s)W(s) - A(s)B(s)Y(s)$$

$$Y(s) = \frac{A(s)W(s)}{1 + A(s)B(s)}$$

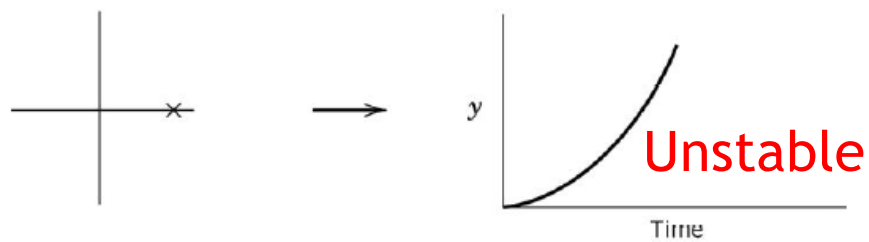
Unstable if any roots of  
 $1 + A(s)B(s) = 0$   
are in right-half of the s-plane:  
exponential growth  $\exp(st)$



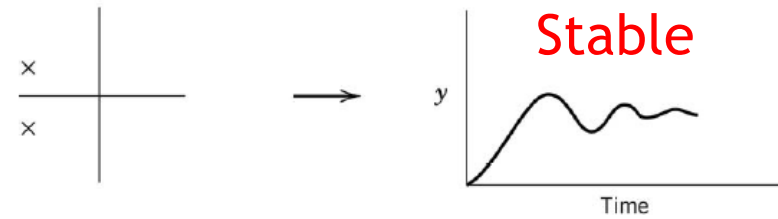
# Stable and unstable behavior



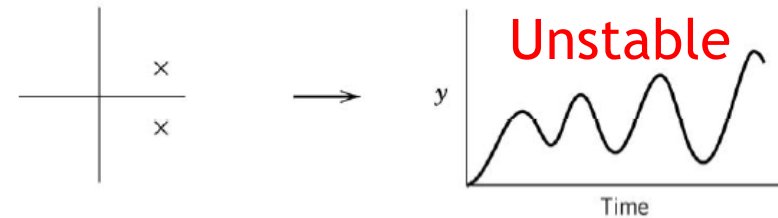
(a) Negative real root



(b) Positive real root

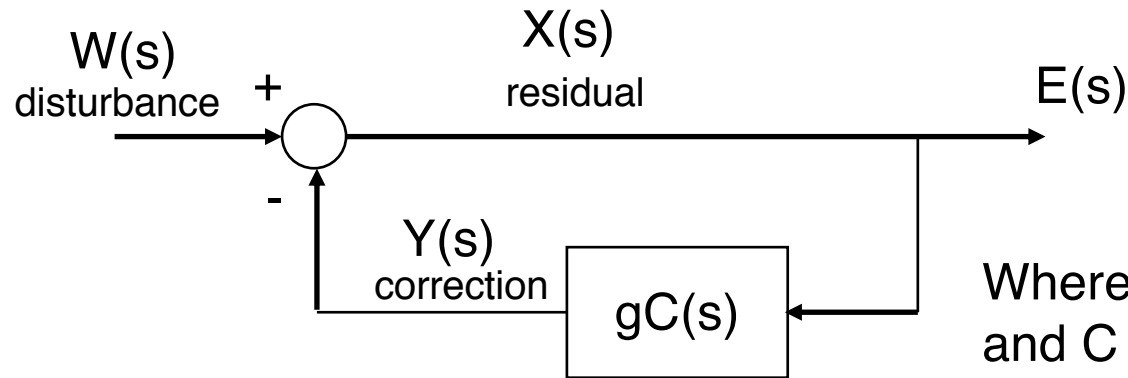


(c) Complex roots (negative real parts)



(d) Complex roots (positive real parts)

# Closed loop control (simple example, $H(s)=1$ )



Where  $g$  is the “gain” and  $C$  is the control law

Our goal will be to suppress  $X(s)$  (residual) by high-gain feedback so that  $Y(s) \sim W(s)$

$$E(s) = W(s) - gC(s)E(s)$$

solving for  $E(s)$ ,

$$E(s) = \frac{W(s)}{1 + gC(s)}$$

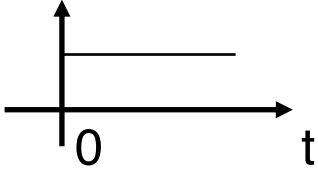
Note: for consistency “around the loop,” the units of the gain  $g$  must be the inverse of the units of  $C(s)$ .



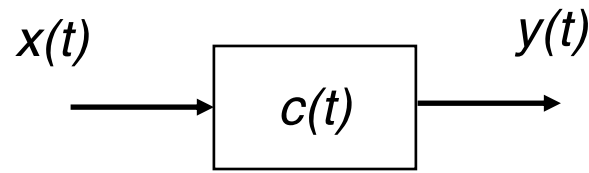
## The *integrator*, one choice for $C(s)$



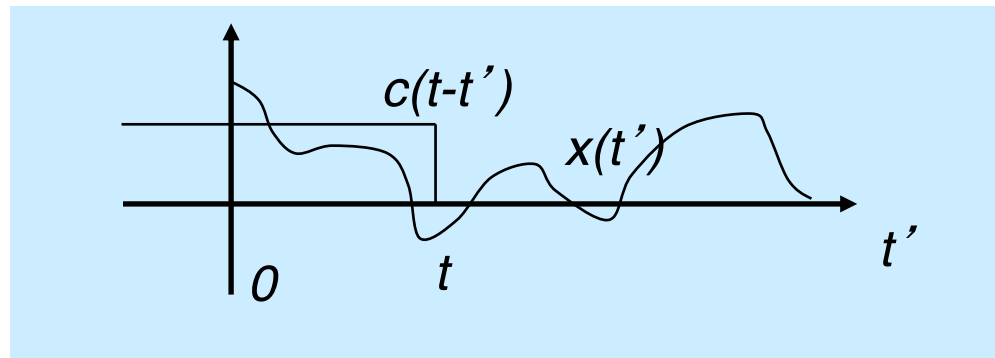
A *system* whose impulse response is the unit step


$$c(t) = \begin{cases} 0 & t < 0 \\ 1 & t \geq 0 \end{cases} \leftrightarrow C(s) = \frac{1}{s}$$

acts as an integrator to the input signal:



$$y(t) = \int_0^t c(t-t')x(t')dt' = \int_0^t x(t')dt'$$

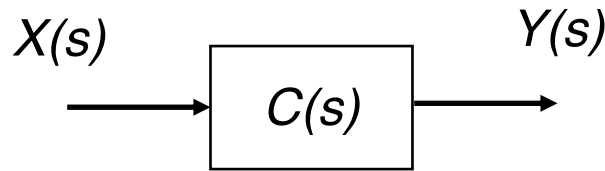


that is,  $C(s)$  integrates the past history of inputs,  $x(t)$

# The Integrator, continued



In Laplace terminology:

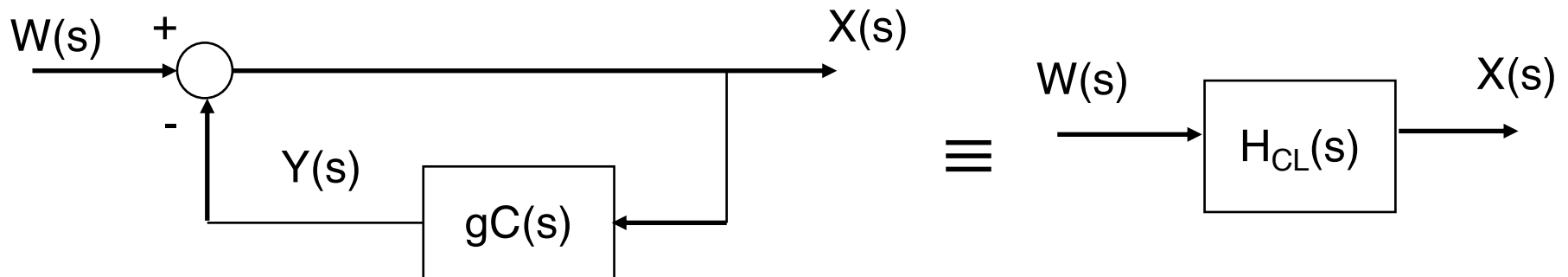


$$Y(s) = \frac{X(s)}{s}$$

An integrator has high gain at low frequencies, low gain at high frequencies.

Write the input/output transfer function for an integrator in closed loop:

The closed loop transfer function with the integrator in the feedback loop is:



$$C(s) = \frac{1}{s} \Rightarrow X(s) = \frac{W(s)}{1 + g/s} = \left( \frac{s}{s + g} \right) W(s) = H_{CL}(s) W(s)$$

closed loop transfer function

output (e.g. residual wavefront to science camera)

input disturbance (e.g. atmospheric wavefront)

## The integrator in closed loop (1)

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$$H_{CL}(s) = \frac{s}{s + g}$$

$H_{CL}(s)$ , viewed as a sinusoidal response filter:

$$H_{CL}(s) \rightarrow 0 \quad \text{as} \quad s \rightarrow 0 \quad \text{DC response} = 0$$

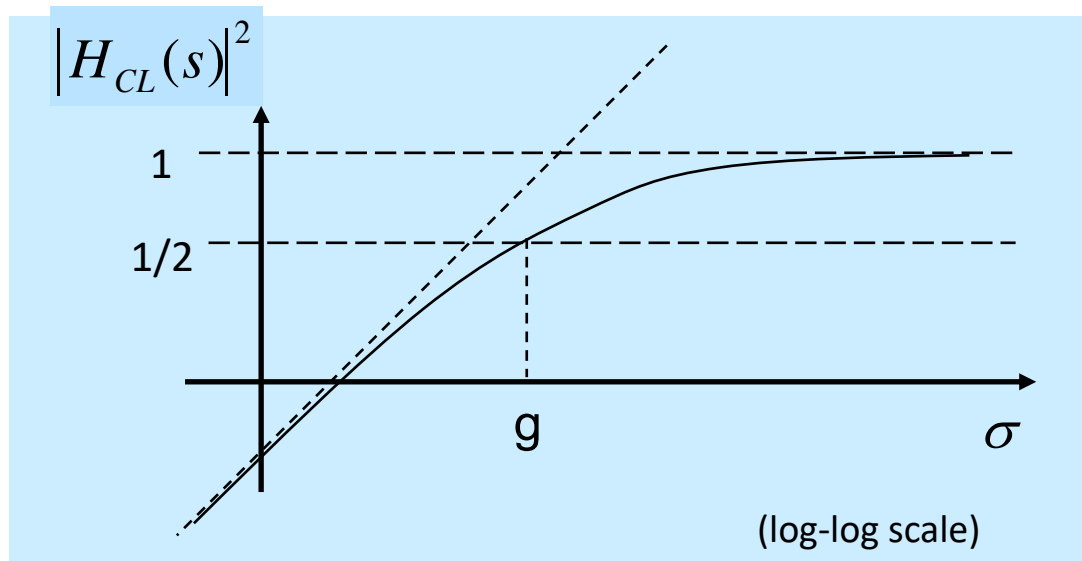
(“Type-0” behavior)

$$H_{CL}(s) \rightarrow 1 \quad \text{as} \quad s \rightarrow \infty \quad \text{High-pass behavior}$$

and the “break” frequency (transition from low freq to high freq behavior) is around  $\sigma \sim g$

## The integrator in closed loop (2)

The break frequency is often called the “half-power” frequency



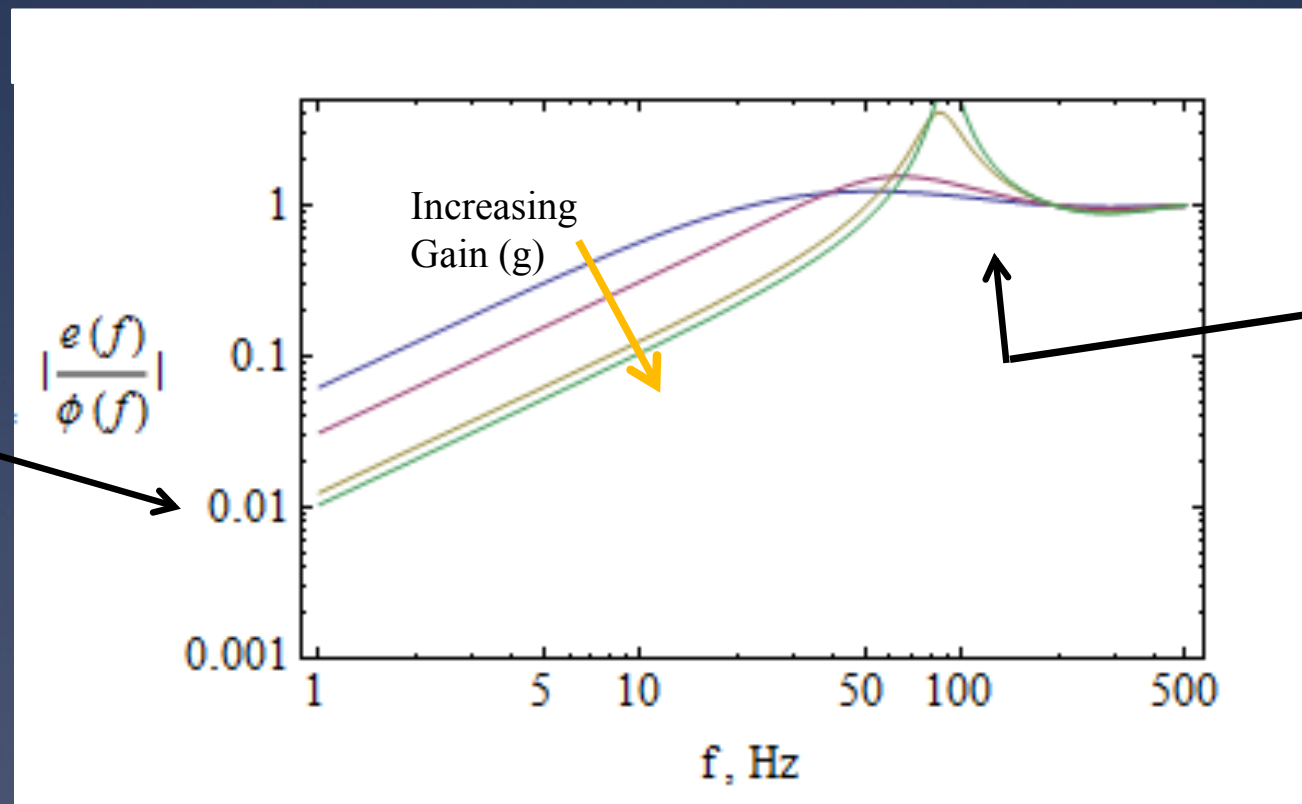
$$H_{CL}(s) = \frac{s}{s + g}$$

- Note that the gain,  $g$ , is the *bandwidth* of the controller:
  - Frequencies below  $g$  are rejected, frequencies above  $\gamma$  are passed.
  - By convention,  $g$  is known as the **gain-bandwidth product**.

# Disturbance Rejection Curve for Feedback Control With Compensation



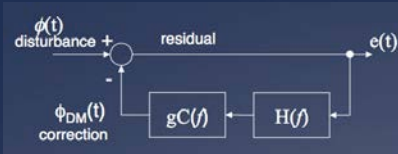
- Controller: element whose role is to maintain a physical quantity in a desired level.
- Compensator : modification of system dynamics, to improve characteristics of the open-loop system so that it can safely be used with feedback control.



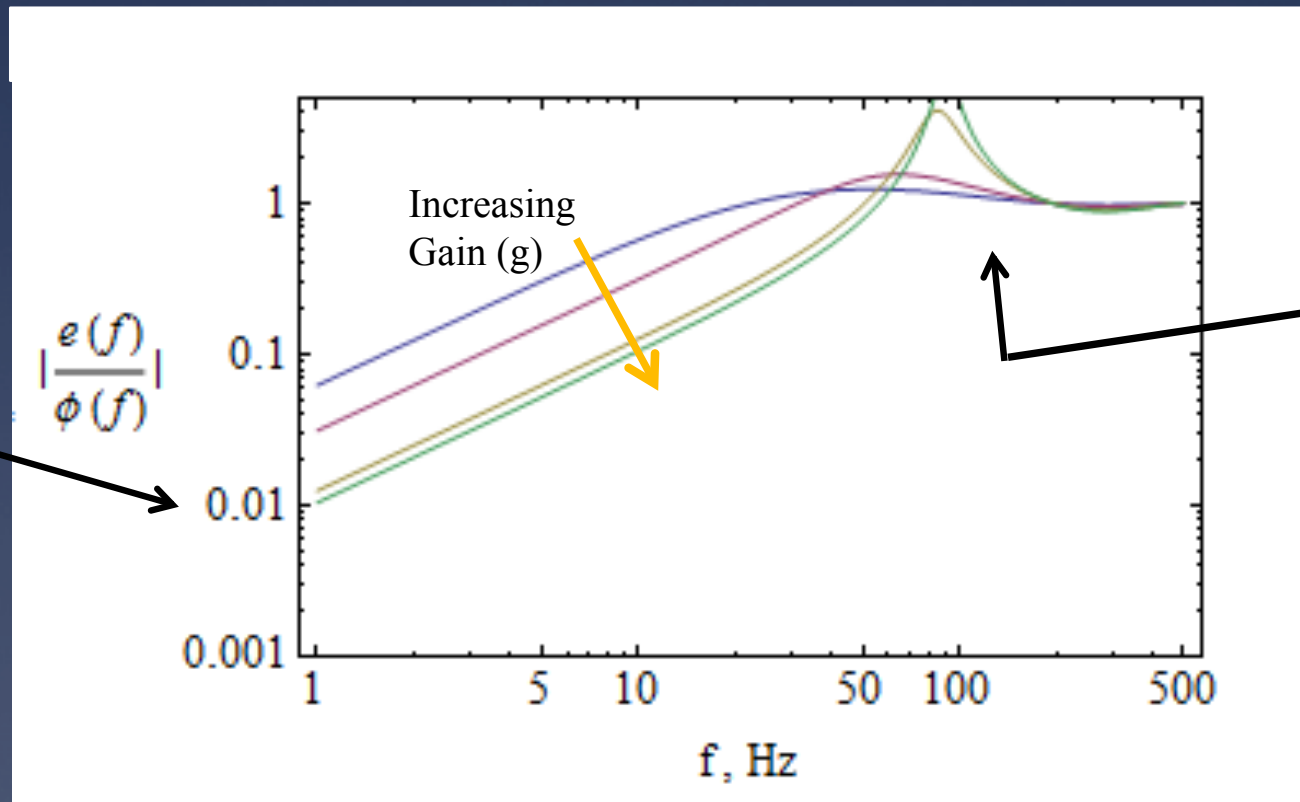
Much better rejection

Starting to resonate

# Disturbance Rejection Curve for Feedback Control With Compensation



$$\frac{e(f)}{\phi(f)} = \frac{1}{1 + gC(f)H(f)}$$



Much better rejection

Starting to resonate

# *Assume that residual wavefront error is introduced by only two sources*

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1. Failure to completely cancel atmospheric phase distortion
2. Measurement noise in the wavefront sensor

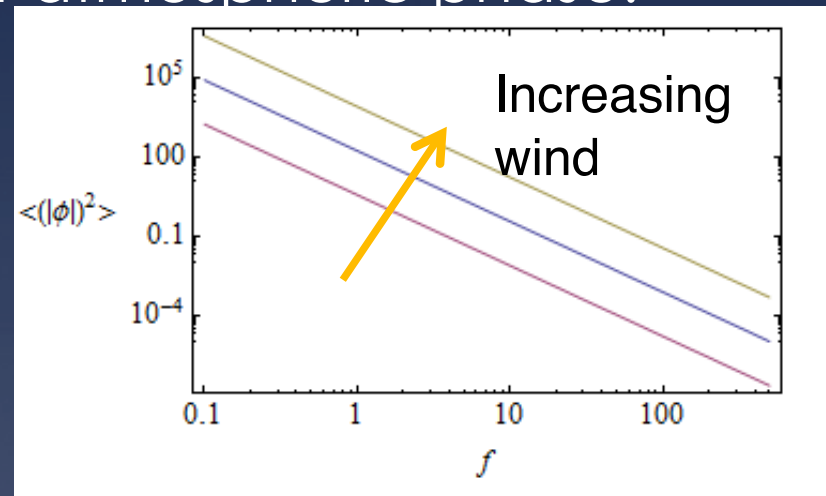
Optimize the controller for best overall performance by varying design parameters such as gain and sample rate

# Atmospheric turbulence



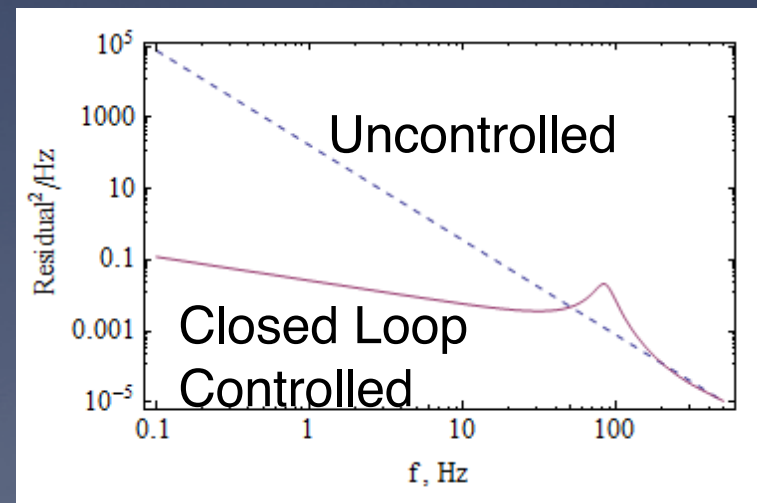
- \* Temporal power spectrum of atmospheric phase:

$$S_{\phi}(f) = 0.077 (v/r_0)^{5/3} f^{-8/3}$$



- \* Power spectrum of residual phase

$$S_e(f) = |1/(1 + g C(f) H(f))|^2 S_{\phi}(f)$$

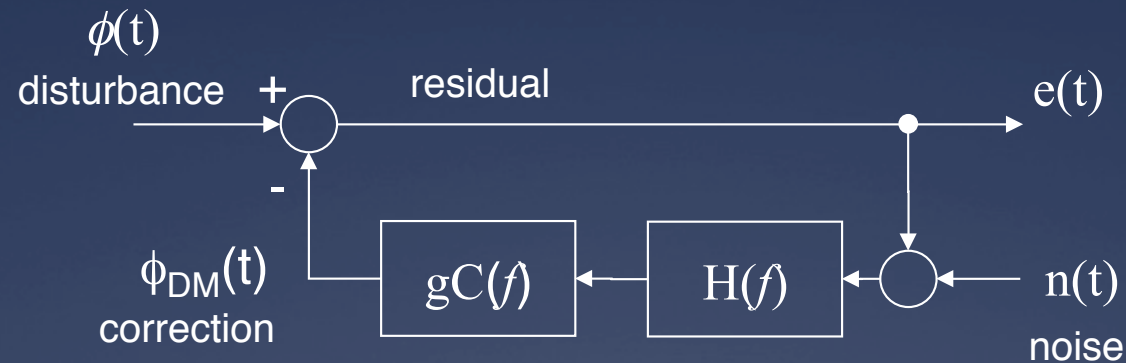




# Noise

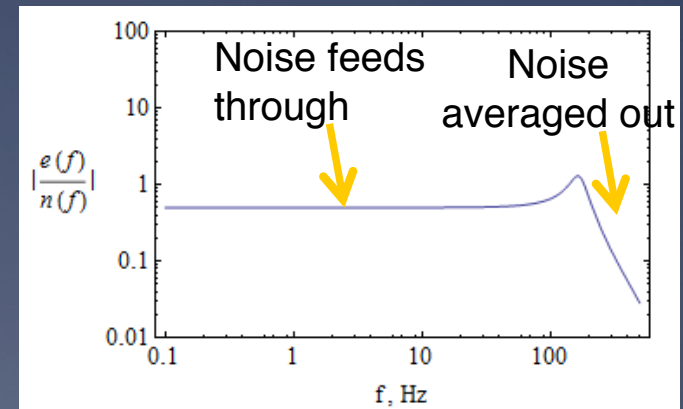


- \* Measurement noise enters in at a different point in the loop than atmospheric disturbance



- \* Closed loop transfer function for noise:

$$e(f) = \frac{gC(f)H(f)}{1 + gC(f)H(f)} n(f)$$

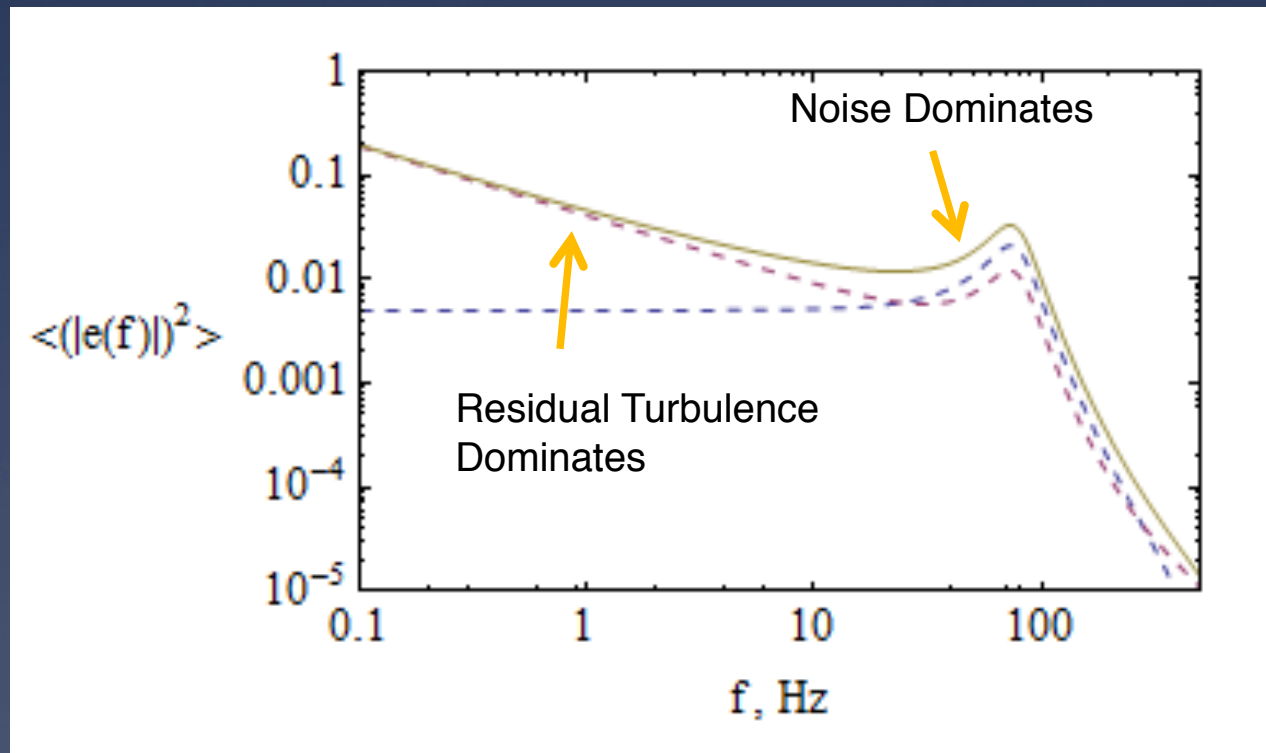


# Residual from atmosphere + noise



## \* Conditions

- \* RMS uncorrected turbulence: 5400 nm
- \* RMS measurement noise: 126 nm
- \* gain = 0.4

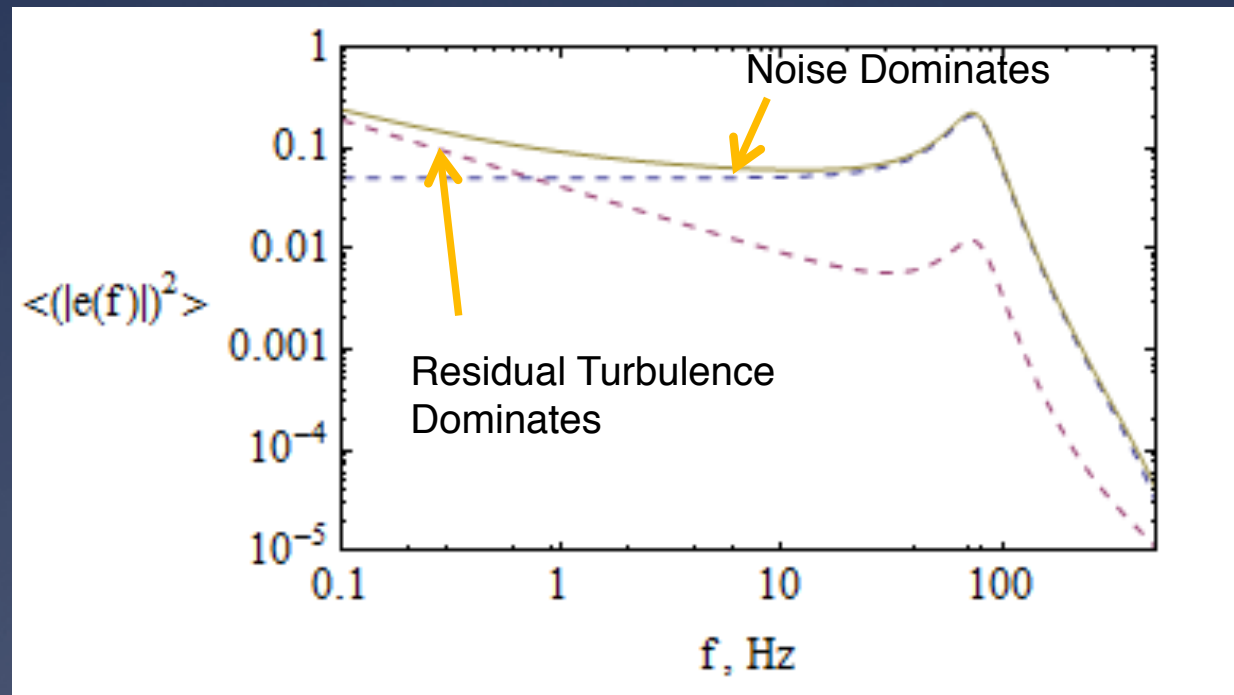


- \* Total Closed Loop Residual = 118 nm RMS

# Increased Measurement Noise



- \* Conditions
  - \* RMS uncorrected turbulence: 5400 nm
  - \* RMS measurement noise: 397 nm
  - \* gain = 0.4



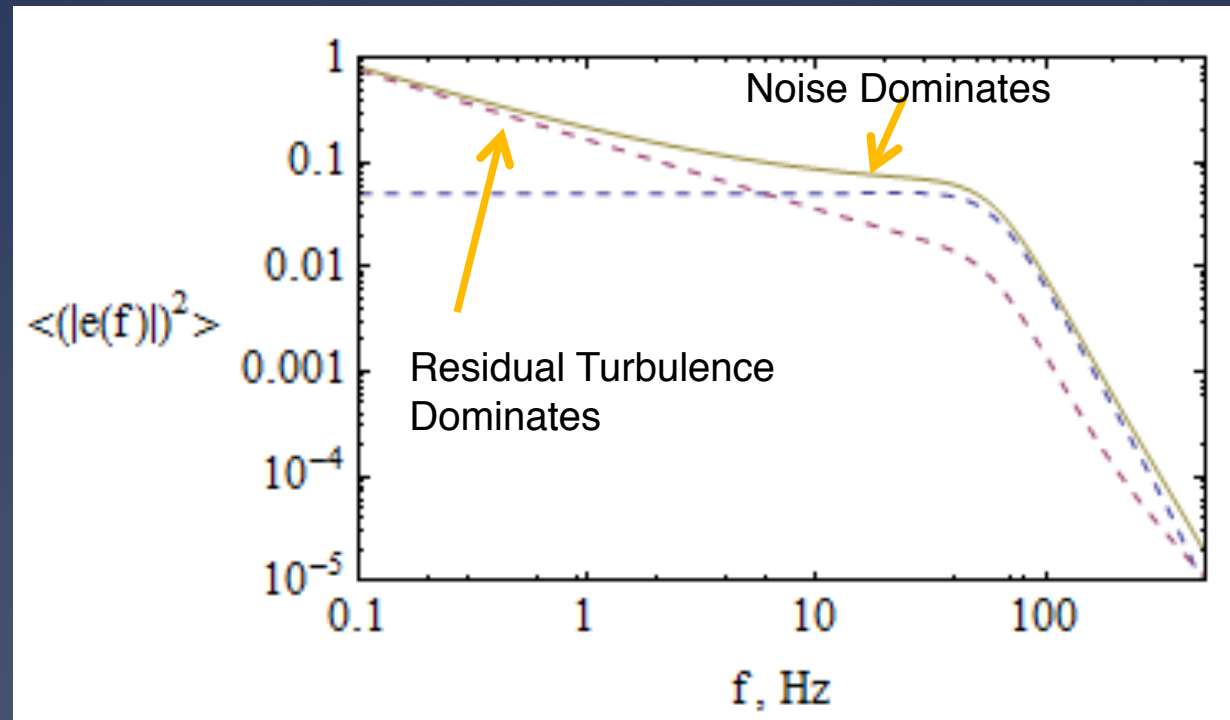
- \* Total Closed Loop Residual = 290 nm RMS

# Reducing the gain in the higher noise case improves the residual



## \* Conditions

- \* RMS uncorrected turbulence: 5400 nm
- \* RMS measurement noise: 397 nm
- \* gain = 0.2



- \* Total Closed Loop Residual = 186 nm RMS

# *What we have learned*

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- Pros and cons of feedback control systems
- The use of the Laplace transform to help characterize closed loop behavior
- How to predict the performance of the adaptive optics under various conditions of atmospheric seeing and measurement signal-to-noise
- A bit about loop stability, compensators, and other good stuff

# References

We have described feedback control only for AO systems.

For an introduction to control of general systems, some good texts are:

G. C. Goodwin, S. F. Graebe, and M. E. Salgado, “Control System Design”, Prentice Hall, 2001

G. F. Franklin, J. D. Powell, and A. Emami-Naeini, “Feedback Control of Dynamic Systems”, 4th ed., Prentice Hall 2002.

For further information on control systems research in AO, see the CfAO website publications and their references.